

Application No. 10/602,128  
Amendment. dated January 26, 2005  
Reply to Office Action of November 26, 2004

### AMENDMENTS TO THE SPECIFICATION

Please replace paragraph 29 with the following amended paragraph:

--In Table 1, the radius, thickness, diameter, and separation dimensions are given in millimeters. Roman numerals identify the lens elements in their respective order from the eyepoint side to the object side.  $n_d$  represents the refractive index of each element;  $v_d$  is the abbe dispersion number;  $R_1$ ,  $R_2$ , etc. represent the radii of the respective refractive surfaces in order, from the eyepoint side to the object side;  $D_1$ ,  $D_2$ , etc. represent the maximum clear lens aperture diameters of the parent lens elements; and  $S_1$ ,  $S_2$  represent the air space between the elements, measured along the optical centerline. In this example, lens element I represents a zero-power eyeglass lens having a base curve of six diopters. It will be recognized by those skilled in the art that other eyeglass lenses may be substituted for the selected eyeglass lens, with minimal affect on the performance of the magnification loupe.--

Please replace paragraph 35 with the following amended paragraph:

--In Table 2, the radius, thickness, diameter, and separation dimensions are given in millimeters. Roman numerals identify the lens elements in their respective order from the eyepoint side to the object side.  $n_d$  represents the refractive index of each element;  $v_d$  is the abbe dispersion number;  $R_1$ ,  $R_2$ , etc. represent the radii of the respective refractive surfaces in order, from the eyepoint

Application No. 10/602,128  
Amendment, dated January 26, 2005  
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side to the object side;  $D_1$ ,  $D_2$ , etc. represent the maximum clear lens aperture diameters of the parent lens elements; and  $S_1$ ,  $S_2$  represent the air space between the elements, measured along the optical centerline.--

Please replace paragraph 38 with the following amended paragraph:

--While the magnification loupes 12, 50 of the present invention have been shown and described having non-circular objective lenses 34, 64, it will be recognized that the loupes may be alternatively manufactured with circular lenses as shown in FIGS. 4A-4B. In particular, the optical loupe depicted in FIG. 4A is configured to be used with a flip-up mounting member 20, as described above for the magnification viewer of FIG. 1. The magnification loupe shown in FIG. 4B is configured to be mounted through the eyeglass lenses 18 of a magnification viewer [[10b]] 10a as described above with respect to FIG. 2. In FIGS. 4A-4B, features similar to the features of magnification loupes 12, 50 of FIGS. 3A-3B are similarly numbered. Specifically, features 12a, 30a, 34a, and 50a, 54a, and 64a correspond to features 12, 30, 34 and 50, 54, and 64 shown and described with respect to FIGS. 3A and 3B.--

Application No. 10/602,128  
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Please replace Table 1 with the following replacement table:

**Table 1**

**Flip-up**

Element	Glass	$n_d$	$v_d$	Radius	Thickness	Max Diameter	Sep.
I	Schott NSK5	1.589	61.3	$R_1 = 98.19$ $R_2 = 98.19$	3.0	25.4	
II	Schott NBALF4	1.580	53.9	$R_3 = 52.10$ $R_4 = 20.16$	1.5	$D_1 = 13.00$ $D_2 = 13.25$	$S_1 = 4.1$
III	O'Hara STIH23	1.785	26.3	$R_5 = 85.68$ $R_6 = 43.17$	1.8	26.15	$S_2 = 13.59$ [[9]]
IV	Schott NBK7	1.517	64.2	$R_7 = 43.17$ $R_8 = 22.39$	7.6	26.15	

Application No. 10/602,128  
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Please replace Table 2 with the following replacement table:

Table 2

Through-the-lens

Element	Glass	$n_d$	$v_d$	Radius	Thickness	Max Diameter	Sep.
I	Schott NSK5	1.589	61.3	$R_1 = \infty$ $R_2 = \infty$	2.2	12.0	
II	Schott NBK7	1.517	64.2	$R_3 = 36.49$ $R_4 = 18.48$	1.5	12.0	$S_1 = 0.6$
III	Schott NSF56	1.805	25.4	$R_5 = 85.68$ $R_6 = 39.71$	1.6	$D_1 = 22.24$ $D_2 = 23.60$	$S_2 = 14.46$ [[6]]
IV	Schott NBK7	1.517	64.2	$R_7 = 39.71$ $R_8 = 21.55$	6.65	$D_3 = 23.60$ $D_4 = 23.60$	